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54 **Support for dynamoelectric machine stator coil end portions.**

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**FR-A- 2 320 653**  
**FR-A- 2 329 094**  
**US-A- 3 348 085**  
**US-A- 3 842 303**  
**US-A- 3 949 256**

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## Description

This invention relates to dynamoelectric machine end turn support arrangements.

There has in the past been and there continues to be a need for improving the bracing of the end turn portions of the winding coils extending from the ends of the stators of dynamoelectric machines such as large turbine generators. Manifestly, the stresses imposed during operation, particularly those caused by vibration, result in wear of coil insulation and fatigue cracking of series and copper strand phase connections. Many proposals have been made in the past in an effort to solve this long standing problem and examples of prior arrangements are illustrated in FR-A-2 329 094 and in United States Patent specifications Nos. 3,949,256; 3,949,257; 4,379,243; and 4,488,079.

The increasing use of four pole machines has exacerbated the problem as a result of the natural vibrational phenomena encountered with such machines. The present invention is aimed at the provision of a more rigid end turn structure which resists such vibrational tendencies.

To alleviate the prior art problems discussed above, the present invention provides a coil support arrangement for use in connection with a dynamoelectric machine equipped with a stator having top and bottom winding coil end portions extending outwardly from the stator at each end thereof. In such machines the coil end portions are generally arranged in phase groups. The support arrangement comprises a support ring encircling the bottom winding coil end portions; respective end blocking means providing lateral support for the coil end portions of each phase group to restrain vibrational movement of the latter during machine operation; and banding means encircling the coil end portions of a phase group, said respective end blocking means and said support ring for holding the coil end portions, the blocking means and the support ring together with the blocking means disposed in axial alignment with the ring, to thereby present a single, blocked, elongated phase group structure which extends circumferentially around the inside of the ring. In accordance with the invention, the blocking means comprises a plurality of individual block elements which are disposed in axial alignment with the ring and which extend the full radial depth of the phase group structure to provide deep beam strength characteristics to the structure.

In a preferred form of the invention the holding means comprises banding means extending longitudinally of the structure across the top surfaces of the top coil end portions, down each end of the structure and around the ring at each end of the structure. Preferably, the holding means comprises

cross banding means extending laterally around the structure and over the longitudinal banding means for tightening the latter by pulling it down to the top of the structure. In a particularly preferred form of the invention, a full depth block element is positioned at each end of the structure and at least one additional full depth block element is positioned centrally of the structure. Ideally, the additional full depth block element should be trapezoidal in shape to facilitate wedging of the same between adjacent top coil end portions and adjacent bottom coil portions.

In practical form, the coil support arrangement of the present invention comprises a plurality of blocked and banded phase group structures disposed in side-by-side relationship around the supporting ring with wedge means disposed between the ends of adjacent structures for applying circumferentially direct tightening forces to the overall arrangement.

The invention also provides an improved dynamoelectric machine which includes the novel support arrangement outlined above.

The invention will become more readily apparent from the following description of a preferred embodiment thereof shown, by way of example only, in the accompanying drawings, wherein:

Figure 1 is a side view of a stator coil end turn assembly at the exciter end of a dynamoelectric machine which incorporates a coil support arrangement in accordance with the concepts and principles of the present invention;

Figure 2 is a sectional view taken along the line 2-2 of Figure 1;

Figure 3 is a cross-sectional view similar to Figure 2 except of the opposite end of the stator; and

Figure 4 is a detail view of wedge means in position between adjacent group structures for tightening the overall assembly.

The winding coil end portions of a stator for a dynamoelectric machine, in this case a large turbine generator, are illustrated in Figure 1 where a top coil end portion is identified by the reference numeral 10, a bottom coil end portion is identified by the reference numeral 12 and a series connection for interconnecting a top coil 10 and a bottom coil 12 is identified by reference numeral 14. Also illustrated in Figure 1 is a phase lead 16 for carrying current from the end of the stator winding in a manner which is well known. Top portion 10 and bottom portion 12 extend outwardly from the end of the stator 18, only a small portion of which is shown.

As is well known to those working in the dynamoelectric machine field, stator 18 and the end portions of the coils, which is conventionally referred to as the diamond area, are annular and

define a bore for the rotor. Traditionally in the dynamoelectric machine art, the winding coil which is closest to the center of rotation of the rotor is referred to as a top coil while the coil element which is furthest from the center of rotation of the rotor is referred to as the bottom coil. Thus, Figure 1 is a cross-sectional elevation view taken essentially at the lower end of the end turn or diamond area of the machine.

A series of support element designated broadly by the reference numeral 20 are spaced around the end of stator 18. Each element 20 has a notched portion at its outboard end 22 for supporting a support ring 24 which extends around the entire diamond area of the machine and encircles bottom winding coil end portions 12. The elements 20 are conventional and provide support for ring 24 in a manner which is known per se.

As will be appreciated by those skilled in the dynamoelectric machine art, Figure 1 is not a true cross-sectional view since it is well known that bottom coil end portions 12 have a throw in one direction while top coil end portions 10 have a throw in the opposite direction providing a cross-hatched, diamond-shaped appearance. Moreover, at the left-hand end of the view, structure has been removed so as to provide an essential elevational view of one end of a phase group structure 26 constructed in accordance with the present invention.

The construction of structure 26 can best be seen with reference to Figure 2. Structure 26 includes a complete phase group, in this case consisting of three top coil end portions 10 and three bottom coil end portions 12. The right-hand most lower end portion 12 is connected to a phase lead 16 as illustrated in Figure 1 and the left-hand most top end portion 10 is connected similarly to a phase lead which is not shown in the drawings. As can be seen viewing Figure 2, the coil end portions which are connected to the phase leads are offset in a conventional manner from the other coils of the phase group.

Structure 26 includes end blocking means consisting of phase blocks 28 and 30 and series blocks 32, 34 and 36. As can be seen viewing Figure 2, block 32 extends essentially for the full radial depth of structure 26, from ring 24 to a position essentially in alignment with top surfaces 10a of coil portions 10. Likewise the left-hand portion 28a of block 28 and the right-hand portion 30a of block 30 extend essentially for the full radial depth of structure 26. Block 32 is trapezoidal in shape to facilitate the arcuate shape of structure 26 which, as can be seen viewing Figure 2, is elongated and extends circumferentially of ring 24. The trapezoidal shape of block 32 also facilitates the insertion of the same by wedging between adjacent

top coil end portions 10 and adjacent bottom coil end portions 12 during the assembly of phase group structure 26.

Means in the nature of phase group banding 38 and cross bands 40 through 52 is provided for holding the coil end portions 10 and 12 of a phase group, the related end blocks 28 through 36 and support ring 24 together to present a block phase group structure 26. As can be seen viewing Figure 1, structure 26 is disposed essentially in axial alignment with ring 24.

Banding 38 extends longitudinally of structure 26 across the top surfaces 10a of top coil end portions 10, down the opposite sides of structure 26 and around ring 24. As can be seen in Figure 2, portions 38a and 38b of band 38 are rotated approximately 90° to facilitate passage around ring 24.

During the assembly of structure 26, series blocks 32, 34 and 36 are driven between the corresponding coil end portions 10 and 12. In this regard, it should be noted that series block 34 is a short series block and is disposed between two adjacent portions 10, whereas series block 36, which is also a short series block, is disposed between a pair of adjacent end portions 12. On the other hand, block 32 extends for the full depth of the structure and is disposed between two adjacent end portions 10 and also between two adjacent end portions 12.

Thus, as can clearly be seen in Fig. 2, block 32 is wedged between a pair of circumferentially spaced top coil end portions 10 and also between a pair of circumferentially spaced bottom coil end portions 12.

Prior to wedging blocks 32, 34 and 36 into position, the same are preferably wrapped in a conventional manner with a piece of dacron felt material 54 which has been filled with a thixotropic thermosetting, curable resin. Blocks 32, 34 and 36 are placed in axial alignment with ring 24 and a resin filled dacron spacer 57 is interposed between ring 24 and the bottom surfaces of coil end portions 12 and blocks 32 and 36. The phase blocks 28 and 30 are positioned as shown in Figure 2 with a piece of resin impregnated dacron felt 56 disposed between each block and the adjacent coil end portion 10 or 12 as the case may be. Block 30 is provided with a similar shelf 30b for accommodating the right-hand bottom coil portion 12 and block 36. Notches 28c and 30c are provided to accommodate felt spacer 57 as shown.

After all of the blocks and impregnated felt members are in position, the banding 38 is wrapped around the entire group structure 26. The band at this stage is simply hand tightened and preferably as many as five layers of banding may be applied. The banding preferably consists of a

polyester glass resin filled band material of a sort which is commonly utilized for such purposes. After each layer of banding is in place the same may conveniently be brushed with a curable resin material. At this stage it may be convenient to place dacron felt spacer members 58 between phase blocks 28 and 30 respectively and ring 24.

As initially installed, band 38 will extend in a straight line from the top right-hand corner to the top left-hand corner of structure 26 due to the arcuate configuration of the top surfaces 10a of coil portions 10 and the top surfaces of the blocks 28, 30, 32 and 34. Cross banding 40 through 52 is now applied as shown. This banding is the same as the banding 38 and again five layers is desirable. Note that holes 28d and 30d are provided in blocks 28 and 30 respectively so that the band at that location can be applied in half sections. That is to say, band 42 goes from opening 28d up and around block 34 and back through hole 28d. Conversely, band 44 goes through hole 28d down and around ring 24 and back up through 28d. The same applies to bands 48 and 50 in the hole 30d.

Bands 40, 46 and 52 go all the way around ring 24 and up and around bands 38 and down again around ring 24. The bands 40, 42, 46, 48 and 52 are pulled tightly, one point at a time, to pull band 38 down against the top surface of structure 26 and thereby tighten band 38. Cinch banding 60 may be used to further support and tighten particularly band 46 as shown. Band 60 may preferably be of the same material and application as other banding described above. In this regard, it should be noted that cinch banding 60 need not go all the way around the block as is shown, but rather holes may be provided in the blocks where desirable to facilitate banding.

After all of the resin material utilized in the spacers and bands has appropriately hardened and cured, the structure 26 will function as a single beam having deep beam strength characteristics by virtue of the fact that blocks 28, 30 and 32 extend for the full radial depth of the structure. Moreover, in the completed structure 26, blocks 28 through 36 provide lateral support for the coil end portions to restrain vibrational movement during machine operation.

The blocking and banding at the turbine end of the stator is illustrated in Figure 3, where structure which is essentially the same as in Figure 2 has been identified with a reference numeral in the 100 series. Thus, ring 124 in Figure 3 is essentially the same and serves the same purpose as ring 24 in Figure 2. The principle difference between the turbine end and the exciter end is that at the former, each top end portion 10 is aligned with a bottom end portion 12 and thus, short series blocks such as the blocks 34 and 36 and intricately configured

group blocks such as the blocks 28 and 30 are not required. Rather, at the turbine end all of the blocks extend for the full radial extent of the structure 126. Thus, the end blocking means at the turbine end consists of series blocks 131 and 133 and phase blocks 128 and 130. In each case, each block provides lateral support for both a top and a bottom coil end portion as shown. Otherwise, the blocked, elongated phase group structure 126 which extends circumferentially of ring 124 at the turbine end of the stator is the same as the blocked, elongated phase group structure 26 which extends circumferentially of ring 24 at the exciter end of the stator. That is to say, structure 126 includes group banding 138, cross banding 141, 143, 145 and 147 and cinch banding 160. Similarly, structure 126 includes impregnated felt members 154 and 156 as well as spacers 157 and 158.

After the structures 26 and 126 have been completed at respective opposite ends of the stator, the entire assemblage may be tightened as illustrated in Figure 4. Figure 4 is a detailed view showing the construction at the exciter end of the stator between adjacent structures 26. This structure includes opposed wedges 62 and 64 which are driven between the phase block 28 on one structure 26 and the phase block 30 on the facing end of the adjacent structure 26. Preferably resin impregnated dacron felt members 66 may be interposed between the wedges and the adjacent surfaces of the structures 26. After assemblage the wedges may be banded with a band 68 (see Figure 2) which extends only around the wedges themselves. Then an external band 70 may be employed to extend around the top of the wedges and down around ring 24, again as shown in Figure 2. The construction at the turbine end for tightening structures 126 is identical with that illustrated in Figure 4.

The blocks 28 through 36, 128, 130, 131 and 133 may be constructed of any material which has sufficient stiffness and other physical characteristics to withstand the conditions in the machine. It has been found, in accordance with the present invention, that an epoxy laminate material is preferable. Such materials are well known in the dynamoelectric machine art and the same may be machined and hand fitted as necessary. This is particularly desirable since the dimensions of the coils and between the coils at the diamond area are not precise. This is also true of the resin filled dacron felt members which provide bases between the blocks and the coil and between the blocks and the support ring. The thicknesses of such members may need to be adjusted from case to case to appropriately provide the necessary support. It has been found that a desirable structure is provided if the dacron felt members are compressed to ap-

proximately 50% of their original thickness after the installation is complete.

It has been found, in accordance with the present invention, and by virtue of the blocks which extend for the full radial depth of the group structures 26 and 126, that each structure acts as though it were a solid, stiff deep beam structure. Thus, the structure is much more resistive of vibrational tendencies than prior structures.

## Claims

1. A coil support arrangement for use in connection with a dynamoelectric machine equipped with a stator (18) having top (10; 110) and bottom (12; 112) winding coil end portions extending outwardly from the stator (19) at each end thereof, said coil portions (10, 12; 110, 112) being arranged in phase groups, said support arrangement being characterized by:

a support ring (24; 124) encircling the bottom winding coil end portions (12; 112);

respective end blocking means (28, 30, 32, 34, 36; 128, 130, 131, 133) providing lateral support for the coil end portions (10, 12; 110, 112) of each phase group to restrain vibrational movement of the coil end portions during machine operation; and

banding means (38, 40, 42, 44, 46, 48, 50, 52, 60; 138, 141, 143, 145, 147, 160) encircling the coil end portions (10, 12; 110, 112) of a phase group, said respective end blocking means (28, 30, 32, 34, 36; 128, 130, 131, 133) and said support ring (24; 124) for holding the coil end portions, the blocking means and the support ring together, with the blocking means (28, 30, 32, 34, 36; 128, 130, 131, 133) disposed in axial alignment with the ring (24; 124), to thereby present a single, blocked, elongated phase group structure (26; 126) which extends circumferentially around the inside of the ring,

said blocking means comprising a plurality of individual block elements (28, 30, 32; 128, 130, 131, 133) which are disposed in axial alignment with the ring and which extend the full radial depth of the phase group structure (26; 126) to provide deep beam strength characteristics to the structure (26; 126).

2. A coil support arrangement according to claim 1, further characterized by the top winding coil end portion having top surfaces and said banding means comprising a banding element (38; 138) extending longitudinally of the structure (26; 126) across the top surfaces (1a; 110a) of the top winding coil end portions (10; 110),

down each end of the structure (26; 126) and around the ring (24; 124) at each end of the structure (26; 126).

3. A coil support arrangement according to claim 2 further characterized by said holding means comprising cross banding means (40, 42, 46, 48, 52; 141, 143, 145, 147) extending laterally around the structure (26; 126) and over the longitudinal banding means (38; 138) for tightening the latter by pulling it down to the top (10a; 110a) of the structure (26; 126).
4. A coil support arrangement according to any of claims 1, 2 or 3, further characterized in that a respective one of block elements (28, 30; 128, 130) which extend the full radial depth of the phase group structure is positioned at each end of the structure (26; 126) and at least one additional block element which extends the full radial depth of the phase group structure (32; 131, 133) is positioned centrally of the structure (26; 126).
5. A coil support arrangement according to claim 4 further characterized in that said additional block element (32; 131, 133) is generally trapezoidal in shape and is wedged between a pair of circumferentially spaced top winding coil end portions (10; 110) and a pair of circumferentially spaced bottom winding coil end portions (12; 112).
6. A coil support arrangement according to any one of claims 1 to 5 further characterized in that a plurality of said phase group structures (26; 126) are disposed in side-by-side relationship around supporting ring (24; 124), said arrangement further comprising wedge means (62, 64) disposed between the ends of adjacent structures (26; 126) for applying circumferentially directed tightening forces to the overall arrangement.

## Patentansprüche

1. Spulentraganordnung zur Verwendung in Verbindung mit einer dynamoelektrischen Maschine, die mit einem Stator (18) ausgestattet ist, der obere (10; 110) und untere (12; 112) Wicklungsspulenendabschnitte aufweist, die sich von dem Stator (18) an jedem Ende nach außen erstrecken, wobei die Spulenabschnitte (10, 12; 110, 112) in Phasengruppen angeordnet sind, wobei die Traganordnung gekennzeichnet ist durch:

einen Tragring (24; 124), der die unteren Wicklungsspulenendabschnitte (12; 112) um-

ringt;

jeweilige Endverblockungsmittel (28, 30, 32, 34, 36; 128, 130, 131, 133), die laterale Unterstützung für die Spulenendabschnitte (10, 12; 110, 112) jeder Phasengruppe bieten, um Vibrationsbewegungen der Spulenendabschnitte während des Maschinenbetriebs einzuschränken; und

Umschnürungsmittel (38, 40, 42, 44, 46, 48, 50, 52, 60; 138, 141, 143, 145, 147, 160), die die Spulenendabschnitte (10, 12; 110, 112) einer Phasengruppe, die jeweiligen Endverblockungsmittel (28, 30, 32, 34, 36; 128, 130, 131, 133) und den Tragring (24; 124) umringen, um die Spulenendabschnitte, die Verblockungsmittel und den Tragring zusammenzuhalten, wobei die Verblockungsmittel (28, 30, 32, 34, 36; 128, 130, 131, 133) in axialer Ausrichtung mit dem Ring (24; 124) angeordnet sind, um dadurch eine einzelne, verblockte, längliche Phasengruppenstruktur (26; 126) zu bilden, die sich umkreisförmig um die Innenseite des Ringes erstreckt,

wobei die Verblockungsmittel eine Vielzahl von individuellen Verblockungselementen (28, 30, 32; 128, 130, 131, 133) aufweisen, die in axialer Ausrichtung mit dem Ring angeordnet sind und die sich über die volle radiale Tiefe der Phasengruppenstruktur (26, 126) erstrecken, um der Struktur (26; 126) in der Tiefe starke Trägereigenschaften zu verleihen.

2. Spulentranganordnung nach Anspruch 1, weiterhin dadurch gekennzeichnet, daß der obere Wicklungsspulenendabschnitt obere Flächen aufweist und daß die Umschnürungsmittel ein Umschnürungselement (38; 138) aufweisen, das sich längs der Struktur (26; 126) über die oberen Flächen (10a; 110a) der oberen Wicklungsspulenendabschnitte (10; 110), an jedem Ende der Struktur (26; 126) abwärts und um den Ring (24; 124) an jedem Ende der Struktur (26; 126) erstreckt.

3. Spulentranganordnung nach Anspruch 2, weiterhin dadurch gekennzeichnet, daß die Haltemittel Kreuzumschnürungsmittel (40, 42, 46, 48, 52; 141, 143, 145, 147) aufweisen, die sich lateral um die Struktur (26; 126) und über das Längsumschnürungsmittel (38; 138) erstrecken, um das Letztere zu spannen, indem es auf die obere Fläche (10a; 110a) der Struktur (26; 126) herabgezogen wird.

4. Spulentranganordnung nach einem der Ansprüche 1, 2 oder 3, weiterhin dadurch gekennzeichnet, daß ein jeweiliges der Verblockungselemente (28, 30; 128, 130) die sich über die

volle radiale Tiefe der Phasengruppenstruktur erstrecken, an jedem Ende der Struktur (26; 126) angeordnet ist und daß zumindest ein zusätzliches Verblockungselement (32; 131, 133), das sich über die volle radiale Tiefe der Phasengruppenstruktur erstreckt, zentral zur Struktur (26; 126) angeordnet ist.

5. Spulentranganordnung nach Anspruch 4, weiterhin dadurch gekennzeichnet, daß das zusätzliche Verblockungselement (32; 131, 133) im wesentlichen trapezförmig ist und zwischen einem Paar von am Umkreis beabstandeten oberen Wicklungsspulenendabschnitten (10; 110) und einem Paar von am Umkreis beabstandeten unteren Wicklungsspulenendabschnitten (12; 112) verkeilt ist.

6. Spulentranganordnung nach einem der Ansprüche 1 bis 5, weiterhin dadurch gekennzeichnet, daß eine Vielzahl der Phasengruppenstrukturen (26; 126) in Nebeneinanderanordnung um den Tragring (24; 124) angeordnet sind, wobei die Anordnung weiterhin Keilmittel (62, 64) aufweist, die zwischen den Enden benachbarter Strukturen (26; 126) angeordnet sind, um in Umkreisrichtung gerichtete Spannkkräfte auf die gesamte Anordnung aufzubringen.

## Revendications

1. Agencement de support de bobine destiné à être utilisé en liaison avec une machine dynamoélectrique munie d'un stator (18) comportant des parties d'extrémité de bobine supérieure (10 ; 110) et inférieure (12 ; 112) s'étendant vers l'extérieur depuis le stator (19) à chaque extrémité de ce dernier, lesdites parties de bobine (10, 12 ; 110, 112) étant disposées en groupes de phase, l'agencement de support susvisé étant caractérisé par :

un anneau-support (24 ; 124) entourant les parties d'extrémité de bobine inférieure (12 ; 112);

des moyens de blocage d'extrémité respectifs (28, 30, 32, 34, 36 ; 128, 130, 131, 133) assurant un support latéral aux parties d'extrémité de bobine (10, 12 ; 110, 112) de chaque groupe de phase pour empêcher le mouvement vibratoire des parties d'extrémité de bobine pendant le fonctionnement de la machine ; et

des moyens de frettage (38, 40, 42, 44, 46, 48, 50, 52, 60 ; 138, 141, 143, 145, 147, 160) entourant les parties d'extrémité de bobine (10, 12 ; 110, 112) d'un groupe de phase, les moyens de blocage d'extrémité respectifs (28, 30, 32, 34, 36 ; 128, 130, 131, 133) et

l'anneau-support (24 ; 124) pour maintenir ensemble les parties d'extrémité de bobine, les moyens de blocage et l'anneau-support, les moyens de blocage (28, 30, 32, 34, 36 ; 128, 130, 131, 133) étant disposés en alignement axial avec l'anneau (24 ; 124) de manière à former ainsi une seule structure (26 ; 126) de groupe de phase allongé et bloqué qui s'étend circonférentiellement le long du côté intérieur de l'anneau,

les moyens de blocage comprenant une pluralité d'éléments individuels formant bloc (28, 30, 32 ; 128, 130, 131, 133) qui sont disposés en alignement axial avec l'anneau et qui s'étendent sur la totalité de l'épaisseur radiale de la structure (26 ; 126) de groupe de phase pour conférer à cette structure (26 ; 126) les caractéristiques de résistance mécanique d'une poutre épaisse.

2. Agencement de support de bobine selon la revendication 1, caractérisé en outre par le fait que la partie d'extrémité de bobine supérieure comporte des surfaces supérieures et que les moyens de frettage comprennent un élément de frettage (38 ; 138) s'étendant dans le sens longitudinal de la structure (26 ; 126) en travers des surfaces supérieures (1a ; 110a) des parties d'extrémité de bobine supérieure (10 ; 110), vers le bas de chaque extrémité de la structure (26 ; 126) et autour de l'anneau (24 ; 124) à chaque extrémité de la structure (26 ; 126).

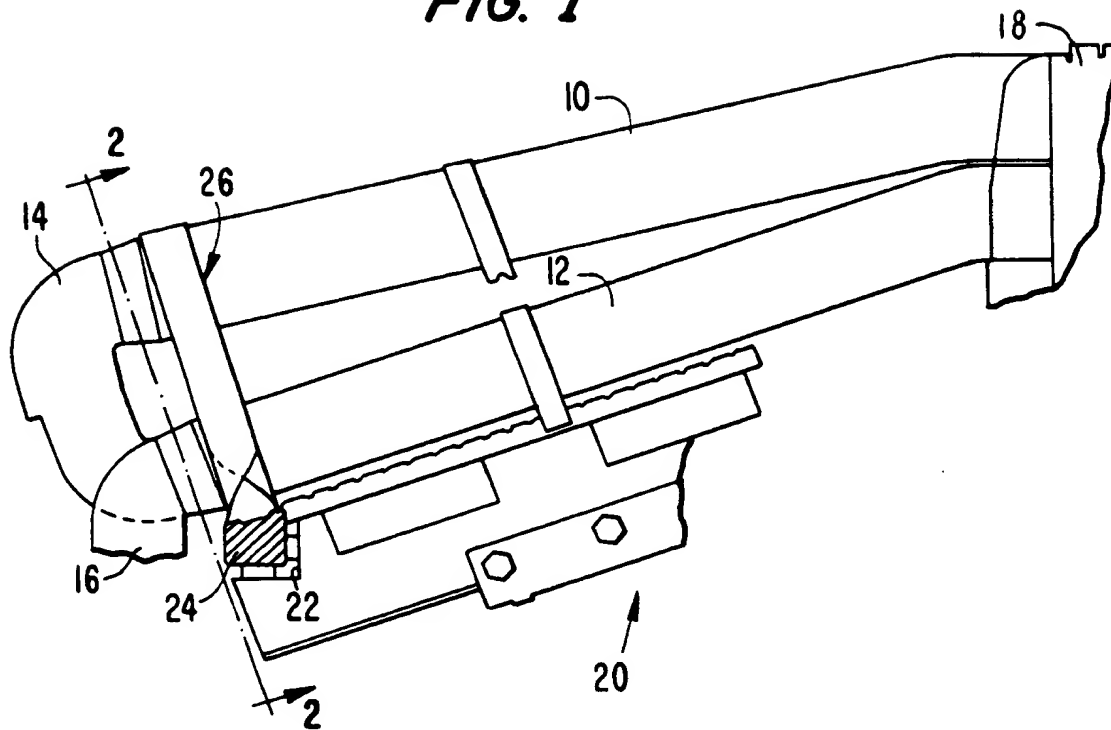
3. Agencement de support de bobine selon la revendication 2, caractérisé en outre par le fait que les moyens de maintien comprennent des moyens de frettage transversaux (40, 42, 46, 48, 52 ; 141, 143, 145, 147) s'étendant latéralement autour de la structure (26 ; 126) et sur les moyens de frettage longitudinaux (38 ; 138) pour serrer ces derniers en les tirant du bas vers le haut (10a ; 110a) de la structure (26 ; 126).

4. Agencement de support de bobine selon l'une quelconque des revendications 1, 2 ou 3, caractérisé en outre par le fait qu'un des blocs (28, 30 ; 128, 130) qui s'étendent sur la totalité de l'épaisseur radiale de la structure de groupe de phase est disposé à chaque extrémité de la structure (26 ; 126) et qu'au moins un bloc supplémentaire qui s'étend sur la totalité de l'épaisseur radiale de la structure (32 ; 131, 133) de groupe de phase est disposé au centre la structure (26 ; 126).

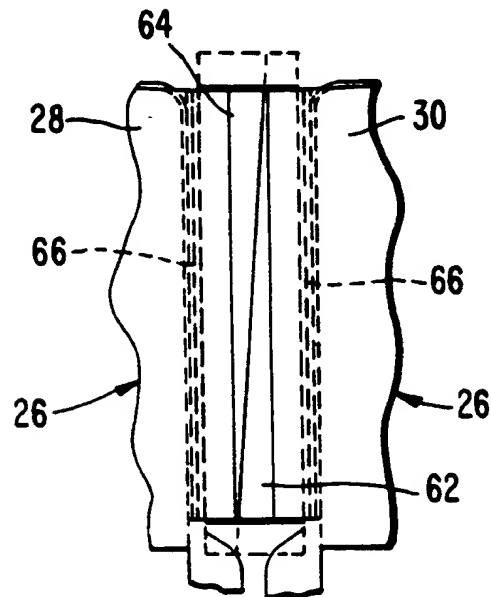
5. Agencement de support de bobine selon la revendication 4, caractérisé en outre par le fait que le bloc supplémentaire (32 ; 131, 133) a une forme trapézoïdale dans son ensemble et qu'il est calé entre une paire de parties d'extrémité de bobine supérieures (10 ; 110) espacées dans le sens circonférentiel et une paire de parties d'extrémité de bobine inférieures (12 ; 112) espacées dans le sens circonférentiel.

6. Agencement de support de bobine selon l'une quelconque des revendications 1 à 5, caractérisé en outre par le fait qu'une pluralité des structures de groupe de phase (26 ; 126) sont disposées côte à côte le long de la circonférence de l'anneau-support (24 ; 124), l'agencement comprenant en outre un moyen formant coin (62, 64) disposé entre les extrémités des structures adjacentes (26 ; 126) pour appliquer des forces de serrage dirigées dans le sens circonférentiel à l'agencement global.

**FIG. 1**

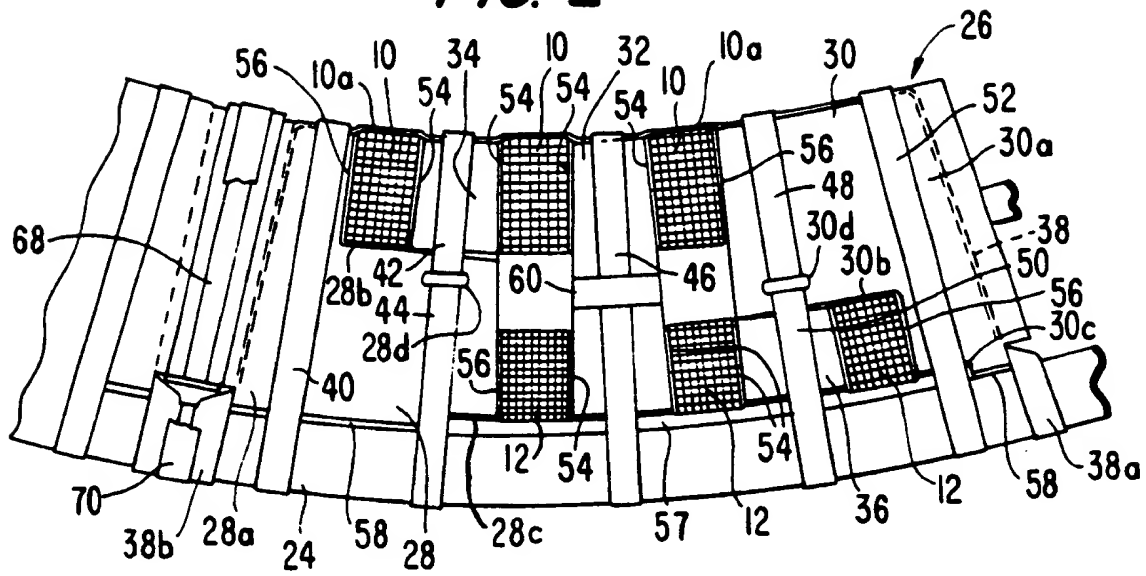


**FIG. 4**





**FIG. 2**



**FIG. 3**

